

1 Article

# 2 Inactivation Rates for Airborne Human Coronavirus by Low 3 Doses of 222 nm Far-UVC Radiation

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12 **Abstract:** Recent research using UV radiation with wavelengths in the 200–235 nm range, often referred to as far-UVC, suggests that the minimal health hazard associated with these wavelengths will allow direct use of far-UVC radiation within occupied indoor spaces to provide continuous disinfection. Earlier experimental studies estimated the susceptibility of airborne human coronavirus OC43 exposed to 222-nm radiation based on fitting an exponential dose-response curve to the data. The current study extends the results to a wider range of doses of 222 nm far-UVC radiation and uses a computational model coupling radiation transport and computational fluid dynamics to improve dosimetry estimates. The new results suggest that the inactivation of human coronavirus OC43 within our exposure system is better described using a bi-exponential dose-response relation, and the estimated susceptibility constant at low doses – the relevant parameter for realistic low dose rate exposures – was  $12.4 \pm 0.4 \text{ cm}^2/\text{mJ}$ , which described the behavior of  $99.7\% \pm 0.05\%$  of the virus population. This new estimate is more than double earlier susceptibility constant estimates that were based on a single-exponential dose response. These new results offer further evidence as to the efficacy of far-UVC to inactivate airborne pathogens.

13 **Keywords:** ultraviolet radiation; far-UVC; coronavirus; airborne; radiation transport; computational fluid dynamics

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## 29 1. Introduction

30 Diseases transmitted through airborne routes have been a public health issue long  
31 before the current COVID-19 pandemic. One of the most prominent and deadly airborne  
32 diseases worldwide is tuberculosis, which was demonstrated to spread via airborne drop-  
33 lets in the 1950s [1]. Other diseases transmitted through airborne routes include measles,  
34 smallpox, influenza [2], and the common cold [3]. Current evidence also points towards  
35 the airborne route for COVID-19 transmission [4]. Undoubtedly, mitigating the risk of  
36 airborne disease transmission is crucial to both current and future public health goals.

37 Vaccination is an effective means of preventing infection from many diseases capable  
38 of spreading through airborne routes; however, vaccine development, testing, produc-  
39 tion, and distribution requires significant time and capital investment [5]. Ultraviolet ra-  
40 diation is an established and viable strategy that can complement vaccination and other  
41 engineering approaches to prevent airborne disease transmission [6]. Because of its non-  
42 targeted mode of action, UV is effective against most airborne pathogens and is likely to  
43 be effective against newly emerging viruses [7]. Crucially, UV differs from the more com-

44 mainly considered approaches to prevent airborne transmission - lockdowns, mask wear-  
45 ing, and vaccination - in that it does not require active decisions on the part of the general  
46 public.

47 Currently, the primary application of ultraviolet radiation for air disinfection is  
48 through upper room ultraviolet germicidal irradiation (UVGI) systems [8]. UVGI systems  
49 typically use lamps emitting primarily at 254 nm. Because direct exposure to 254 nm ra-  
50 diation can potentially cause harm to the eyes and skin, UVGI systems restrict radiation  
51 to the upper portion of the room and are carefully installed to minimize emissions into  
52 human-occupied spaces [9].

53 A new concept in the use of ultraviolet radiation for airborne disinfection utilizes the  
54 wavelength range from 200-235 nm, often referred to as far-UVC [10-15]. Research has  
55 demonstrated these wavelengths are at least as effective for microbial inactivation as con-  
56 ventional 254 nm UV radiation [10, 11, 14-21], yet potentially without the associated health  
57 hazards [10-13, 22-33]. Thus far-UVC can potentially be directly used in occupied indoor  
58 locations to continuously disinfect the air and exposed surfaces [14, 15]. Recent modeling  
59 work has predicted that application of far-UVC within a room can offer an individual  
60 protection against airborne viruses similar to that provided by wearing an N95 mask [34].

61 Our earlier laboratory work demonstrated the efficacy of inactivation of aerosolized  
62 viruses with 222 nm far-UVC, first for airborne influenza A virus H1N1 [15] and, more  
63 recently, for airborne human coronaviruses 229E and OC43 [14]. In the current work we  
64 a) studied a much wider range of far-UVC doses, and b) used a computational model to  
65 generate improved dosimetry estimates. The wider dose range is of particular importance  
66 in that in real-life scenarios the far-UVC exposures will be delivered at very low dose rates  
67 – effectively repeating multiple times the low-dose part of the dose-response relation [35]  
68 – and thus the overall effectiveness will be determined by the low-dose component of the  
69 dose-response relation.

## 70 2. Materials and Methods

### 71 2.1. Viral Strain

72 All experiments were performed using the human coronavirus OC43 (HCoV-OC43)  
73 (ATCC VR-1558). The HCoV-OC43 virus appears to be a suitable surrogate for SARS-  
74 CoV-2, with comparable physical and genomic size [36], and has been previously used by  
75 our group [14] and others [37] for ultraviolet radiation efficacy studies. Recent research  
76 on SARS-CoV-2 susceptibility with 222 nm radiation on surfaces [20, 21] as well as other  
77 studies investigating coronavirus susceptibility [38] provide further evidence of similar  
78 efficacy between coronaviruses. Details of preparation of this virus and its propagation in  
79 host WI-38 normal lung cells (ATCC CCL-75) are available in the manuscript by Bu-  
80 nanno *et al.* (2020)[14].

### 81 82 2.2. Benchtop Aerosol Irradiation Chamber

83 Virus inactivation experiments were performed using our custom-built benchtop  
84 aerosol irradiation chamber. The layout and operation of this system was previously de-  
85 scribed in detail [14, 15]. This one-pass exposure system integrates the generation, expo-  
86 sure, and collection of virus containing aerosols within a single chamber. The benchtop  
87 system includes a nebulizer for aerosol generation, dry and humidified air inputs to main-  
88 tain humidity, particle size monitoring, an exposure volume (279 mm tall x 254 mm wide  
89 x 63 mm deep) with a UV transmitting window to enable UV exposure within the cham-  
90 ber, and a vacuum pump to move the aerosol through the system. Some modifications  
91 have been made to the system since our previous report [14] in order to enable a broader  
92 range of radiant exposure doses and improve overall system operation. First, the chamber  
93 previously used a UV transmitting plastic as the exposure window on the chamber. For  
94 the tests described here, the chamber window is 6 mm of quartz glass (GE Type 124, Tech-  
95 nical Glass Products, Painesville, Ohio). The measured transmission of the 6 mm quartz  
96 window for 222 nm radiation was 72%. Second, the rear reflector used within the chamber

97 is now Anolux UVS aluminum (Anomet, Brampton, Ontario, Canada). Anolux has a specular  
98 reflectance of approximately 60% for 222 nm radiation. Third, aerosol collection was  
99 performed using 37 mm gelatin membrane filters (SKC Inc., Eighty Four, PA, USA) held  
100 within a plastic air monitoring cassette (37 mm SureSeal Cassette, SKC Inc.). Previously  
101 our system utilized a BioSampler (SKC Inc.) for aerosol collection, which also controlled  
102 the flow rate through the chamber to be 12.5 LPM. With the change to gelatin filters for  
103 collection, it was necessary to incorporate a precision flow orifice (B-47-SS, O'Keefe Con-  
104 trols Co, Monroe, CT, USA) which set the flow rate through the system to 11.6 LPM via  
105 choked flow operation conditions using the system vacuum. A vacuum gauge was used  
106 to verify choked flow operating conditions for the orifice, and the flow rate through the  
107 system was monitored with an inline air flow meter (EW-32461-54, Cole-Parmer, Vernon  
108 Hills, IL). Given these system changes, the total time for a particle to traverse the exposure  
109 window was approximately 23 seconds.  
110

### 111 2.3. Irradiation Chamber Performance

112 The overall chamber performance was similar to our previous studies testing efficacy  
113 of aerosolized virus inactivation [14, 15]. The average temperature during testing was  
114 24°C and the relative humidity was between 60-70%. The aerosol size distribution, which  
115 was measured using an optical particle counter (HAL-HPC601, Hal Technology, Rancho  
116 Cucamonga, CA), was again typical of human coughing, breathing, and talking [39], with  
117 over 90% of particles less than 1.0 µm diameter.  
118

### 119 2.4. Far-UVC Lamp and Dosimetry

120 The far-UVC source used in this study was a 12 W 222-nm KrCl excimer lamp module  
121 made by USHIO America (Item #9101711, Cypress, CA). The lamp is equipped with a  
122 proprietary optical filtering window to reduce lamp emissions outside of the 222 nm KrCl  
123 emission peak. Spectral analysis of the filtered KrCl lamp was performed using a Giga-  
124 hertz Optik BTS2048-UV light meter (Gigahertz-Optik Inc, Amesbury, MA) and the nor-  
125 malized emission spectrum is provided in Supplemental Figure S1. The lamp was posi-  
126 tioned 22 cm away from the exposure chamber window and directed at the center of the  
127 window. The intensity of the lamp was measured using a UIT2400 meter (International  
128 Light Technologies, Inc., Peabody, MA, USA) equipped with an SED220 detector and W  
129 diffuser input optic. The lamp intensity data was input into the radiation transport model  
130 to calculate the radiant exposure dose received by particles moving through the system.  
131

### 132 2.5. Computational Model of Exposure System

133 A model incorporating radiation transport and computational fluid dynamics (CFD)  
134 was used to simulate the exposure dose received by particles representing aerosols con-  
135 taining virus as they traveled through the exposure chamber. The general modeling ap-  
136 proach is described in detail elsewhere [34, 40]. The model simulated the experimental  
137 setup, including the chamber geometry, the position and emission pattern of the far-UVC  
138 source, and the flow conditions of the aerosols within the chamber. It resolves the spatially  
139 varying flow fields and far-UVC fluence variations within the chamber and includes a  
140 particle model for aerosol tracking, enabling the calculation of the far-UVC inactivation  
141 of aerosolized human coronavirus in the system. This was achieved by using the WY-  
142 VERN coupled radiation-CFD code [34], a high-fidelity modeling solver for the Boltz-  
143 mann transport and Navier-Stokes (with Large Eddy Simulation(LES)) equations.  
144

145 The simulation tracked 1600 particles, representing virus containing aerosols,  
146 through the irradiation chamber. They were initiated at the chamber's inlet face where  
147 they were evenly distributed in a 40 x 40 grid, and followed the flow field, as predicted  
148 by the model, to the outlet channels. The virus content of a particle was initiated to a unit  
149 value and this decayed according to the strength of the radiation field, at its respective  
position, within the domain.

150 Effects from aerosol size have not been included in this model. Given the very short  
151 time scales within the chamber, the laminar flows, and small sizes of aerosols, the domi-  
152 nating effect driving their transport is via the air flow velocity. Aerosol transport is there-  
153 fore modelled based solely on the airflow. Similarly, aerosol dependent radiation  
154 transport effects such as shadowing and scattering are not considered in this simulation  
155 because of the small size of the aerosols.

## 157 2.6. Experimental Protocol

158 As previously described [14], the virus solution in the nebulizer consisted of 1 ml of  
159 Modified Eagle's Medium (MEM, Life Technologies, Grand Island, NY) containing  $10^6$ -  
160  $10^7$  50% Tissue Culture Infection Dose (TCID<sub>50</sub>) of coronavirus, 20 ml of deionized water,  
161 and 0.05 ml of Hank's Balanced Salt Solution with calcium and magnesium (HBSS++). The  
162 irradiation chamber was operated with aerosolized virus particles flowing through the  
163 chamber and the bypass channel for 5 minutes prior to each experiment. Sample collection  
164 was initiated by changing air flow from the bypass channel to the gelatin filter using the  
165 pair of three way valves. During each sampling time, which lasted for 30 minutes, the  
166 inside of the irradiation chamber was exposed to 222-nm far-UVC light entering through  
167 the quartz window.

168 Variation of the far-UVC dose delivered to aerosol particles was achieved by insert-  
169 ing precision wire meshes between the far-UVC emitting lamp and the exposure chamber.  
170 The wire meshes used in this work had open areas of 64% (item number 9656T11), 46%  
171 (9656T15), or 31% (9656T18); all meshes were purchased from McMaster-Carr (Elmhurst,  
172 IL, USA). Each mesh was confirmed to transmit 222 nm far-UVC in agreement with the  
173 specified open area percentage. The mesh was placed against the quartz window of the  
174 chamber when only a single mesh was required. For exposures using two meshes in series,  
175 the second mesh was placed against the output window of the lamp. Zero-dose control  
176 studies were conducted with the excimer lamp turned off. Some test conditions required  
177 the dose to be altered by reducing the exposure time by 50%; this was done by covering  
178 half of the exposure window with a thick card stock which did not transmit UV radiation.  
179 Combinations of wire meshes and the 50% reduction in exposure time were utilized to  
180 achieve the doses shown in Table 1. After the sampling period was completed, the gelatin  
181 filter was dissolved by shaking in 5 mL of PBS pre-warmed at ~30°C for 5 minutes, and  
182 the solution was used for the virus infectivity assays.

## 184 2.7. Virus Infectivity Assay

185 Testing for inactivation followed the same procedure for testing the 50% Tissue Cul-  
186 ture Infectious Dose (TCID<sub>50</sub>) assay as described in Buonanno *et al.* [14, 41, 42]. Briefly, the  
187 collected viral solution was serially diluted (1:10) and overlaid on WI-38 human lung  
188 cells seeded the day before the experiment in 96-well plates ( $10^5$  cells/well); after a two-  
189 hour incubation period at 33-34°C in infectious medium (MEM + 2% heat-inactivated  
190 FBS), the infectious medium was aspirated and replaced by fresh medium (MEM + 10%  
191 heat-inactivated FBS + pen/strep) and the plate returned to the incubator. Cytopathic ef-  
192 fects (CPE) (e.g., vacuolization of cytoplasm and sloughing) were scored 3 or 4 days later  
193 and TCID<sub>50</sub> was calculated with the Reed-Muench method [41, 43].

## 195 2.8. Data Analysis

196 The two phase dose-response model used in this work is commonly used in disin-  
197 fection and microbial inactivation analyses [7]. This model describes a bi-exponential  
198 dose-response, where one exponential describes the behavior of a susceptible fraction of  
199 the population, and the second exponential describing the response of a more resistant  
200 subpopulation:

$$201 S = (1 - f)e^{-k_1 D} + fe^{-k_2 D}, \quad (1)$$

where  $S$  is the non-inactivated (surviving) fraction of the virus and  $D$  is the radiant exposure dose in  $\text{mJ}/\text{cm}^2$ .  $(1 - f)$  and  $f$  are respectively the proportions of the sensitive and the resistant subpopulations whose exponential dose responses are respectively defined by parameters  $k_1$  and  $k_2$  (units of  $\text{cm}^2/\text{mJ}$ ). The mono-exponential model was described as:

$$S = e^{-kD}. \quad (2)$$

The non-inactivated fraction ( $S$ ) of the virus for each exposure condition was calculated by dividing the  $\text{TCID}_{50}$  at each dose by the  $\text{TCID}_{50}$  of the unexposed condition:  $S = \text{TCID}_{50, \text{UV}} / \text{TCID}_{50, \text{control}}$ . Inactivation values were calculated for each repeat experiment and natural log ( $\ln$ ) transformed to bring the error distribution closer to normal [44]. Robust regression was performed using *R* 4.0.3 software [45] using these normalized  $\ln[S]$  values as the dependent variable and UV dose ( $D$ ,  $\text{mJ}/\text{cm}^2$ ) as the independent variable. The *nls* function in *R* was used to fit the non-linear bi-exponential model (Equation 1), and the *rlm* function was used to fit the linear single-exponential model (Equation 2).

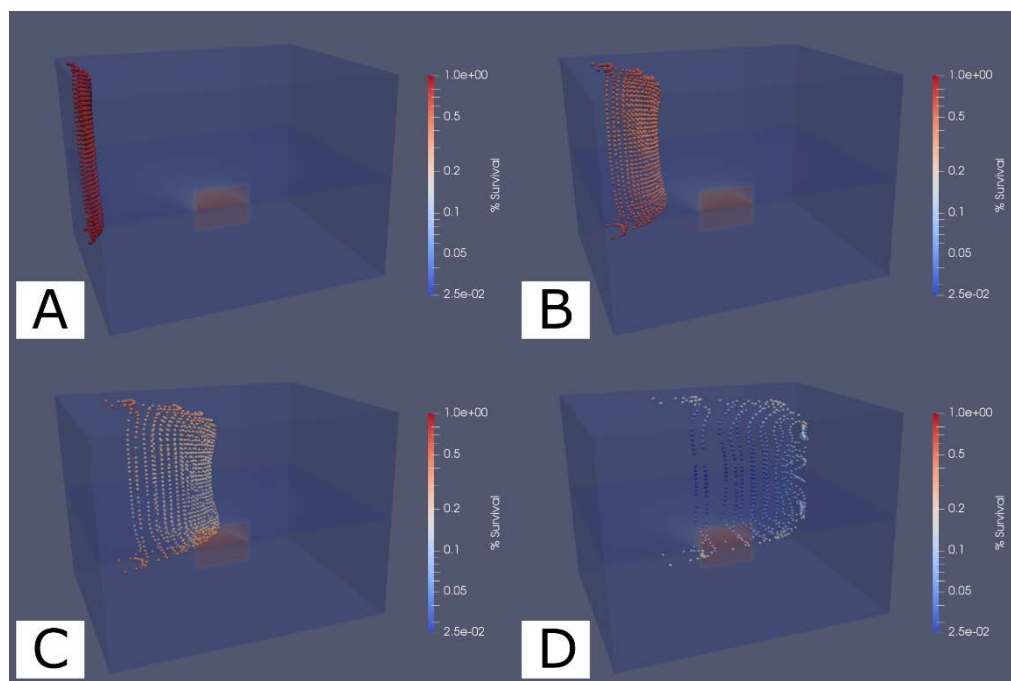
The performances of both model versions (Equations 1 and 2) were compared using the Akaike information criterion with sample size correction (AICc) [46, 47], which compares maximized log likelihood values for all models and penalizes model complexity (*i.e.* extra adjustable parameters). The model with the lowest AICc score is better supported by the data. The “evidence ratio” of each model relative to the other was evaluated using the quantity  $\exp(\Delta\text{AICc}/2)$ , where  $\Delta\text{AICc}$  is the difference in AICc scores between models.

### 3. Results

#### 3.1. Far-UVC Dosimetry

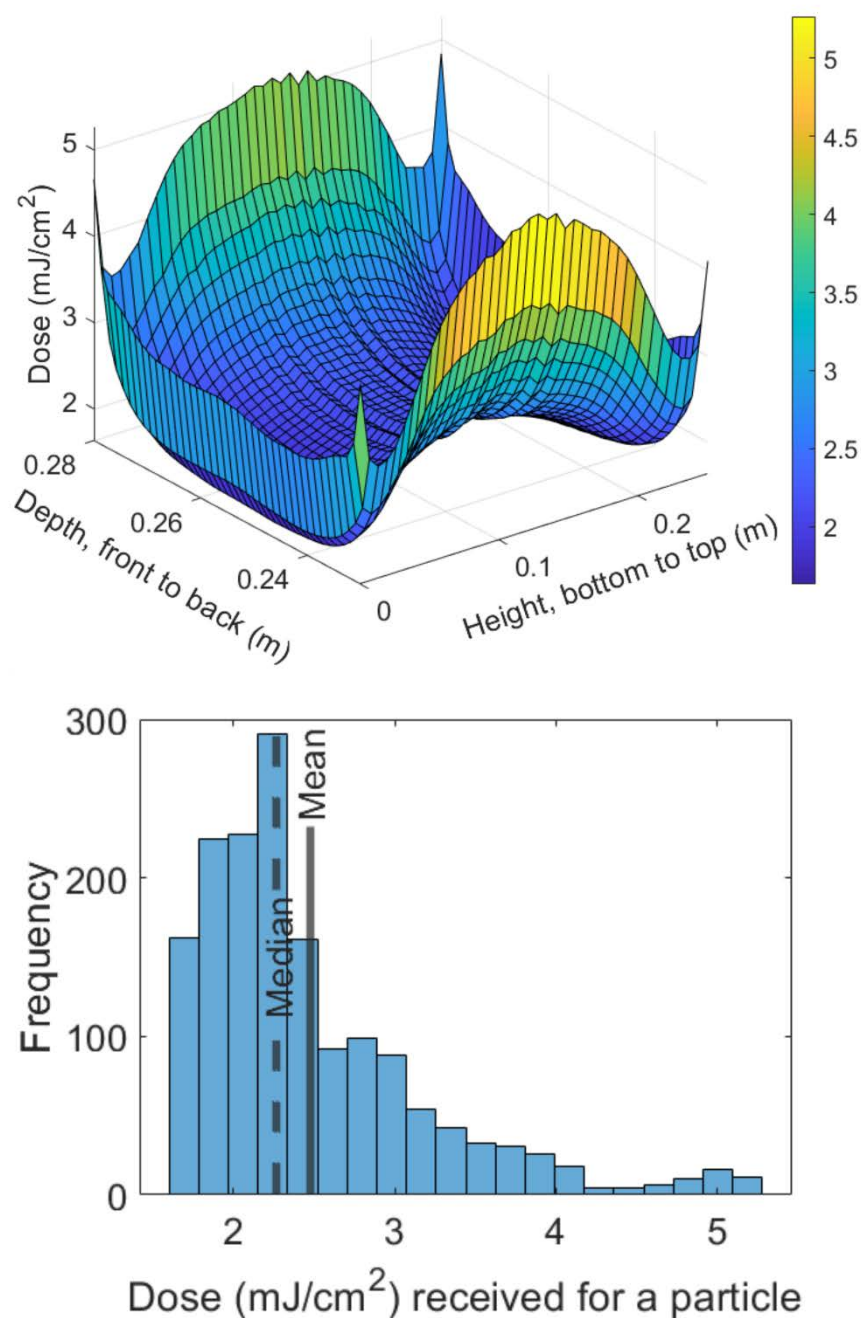
Measurements of the far-UVC lamp angular emission pattern and the intensity change with distance were recorded, and the values were confirmed to be in agreement with the computational radiation transport model for the lamp. Additional details on the validation are available in the previous description of the radiation model [40].

Selected frames from the dosimetry simulation are shown in Figure 1, and a video of the complete simulation showing motion through the chamber is available with the Supplemental Materials. The images in Figure 1 show the lamp position in the foreground emitting towards the UV exposure volume within the chamber at the rear of the simulation volume. The aerosols move from left to right and accumulate dose according to the radiation flux at their position. The aerosol particle streamlines were observed to proceed directly across the chamber, but did converge into the two exit ports for the chambers shortly after leaving the exposure area. The major influence on the aerosol particle streamlines appears to be the friction around the edges of the flow volume since the flow pattern takes a parabolic flow profile (visible in panels B and C of Figure 1) typical of laminar flow conditions. The color change of the aerosol particles in Figure 1 represents the relative survival of virus throughout the exposure.



**Figure 1.** Simulation results of aerosol dosimetry showing the relative survival fraction of virus in aerosols as they traverse across the exposure chamber. Aerosols in the simulation were uniformly distributed across the left side of the exposure volume and released to move through the volume. The aerosol color changing from red to blue indicates an increase in the total radiation flux received by that aerosol over time. Four frames (A-D) show aerosol position at time instance of 2, 6, 10 and 20 seconds from entering the chamber. These frames illustrate the flow pattern as well as the virus inactivation for each aerosol. Panel A shows the aerosol particles evenly distributed as they begin into the exposure volume, and panels B and C show the particles progressing across the exposure volume. Panel D shows many of the particles have reached the two chamber outlet ports on the right side, while slower travelling particles are still being exposed. A video of the simulation result is available in the Supplemental Materials.

The total flux upon each simulated aerosol particle was tracked through the chamber, and the cumulative doses are plotted in Figure 2 in both a surface plot and a histogram. Due to the laminar flow conditions, aerosol particles entering at the same position followed the same path through the chamber, and hence experienced the same radiation exposure and underwent the same virus inactivation. However, aerosol particles entering through different positions at the inlet took different paths through the chamber and experience varying levels of radiation exposure, and hence experience different doses. Consequently, the dose experienced by the virus can be mapped as function of position at the inlet face of the chamber. This is presented in Figure 2 showing a higher dose being received to virus close to the chamber's edges which is a result of the slowing of the fluids and, therefore, extension of the dwell times. The mean and median dose received by a particle for the simulation were respectively  $2.47 \pm 0.71$  mJ/cm<sup>2</sup> and 2.26 mJ/cm<sup>2</sup>. Mean dose was used for modeling of the virus susceptibility.



**Figure 2.** The dose received by the simulated aerosol particles as they travel across the exposure chamber. The surface plot shows the influence of the starting position of the particle to the total dose received. The x-axis on the plot is the depth of the chamber (0.23 m to 0.28 m), which defines the space from the front of the chamber to the back wall of the chamber. The y-axis of the plot is for the height of the chamber. A histogram plot of the frequency of each dose among the 1600 simulated particles indicates that the dose distribution is right skewed.

The different doses delivered to the aerosol particles in the experiment were obtained with a combination of precision wire meshes to reduce the total exposure time by blocking a portion of the total far-UVC exposure. The different mesh blocking combinations are listed in Table 1, along with the range of doses ultimately applied to the aerosol.

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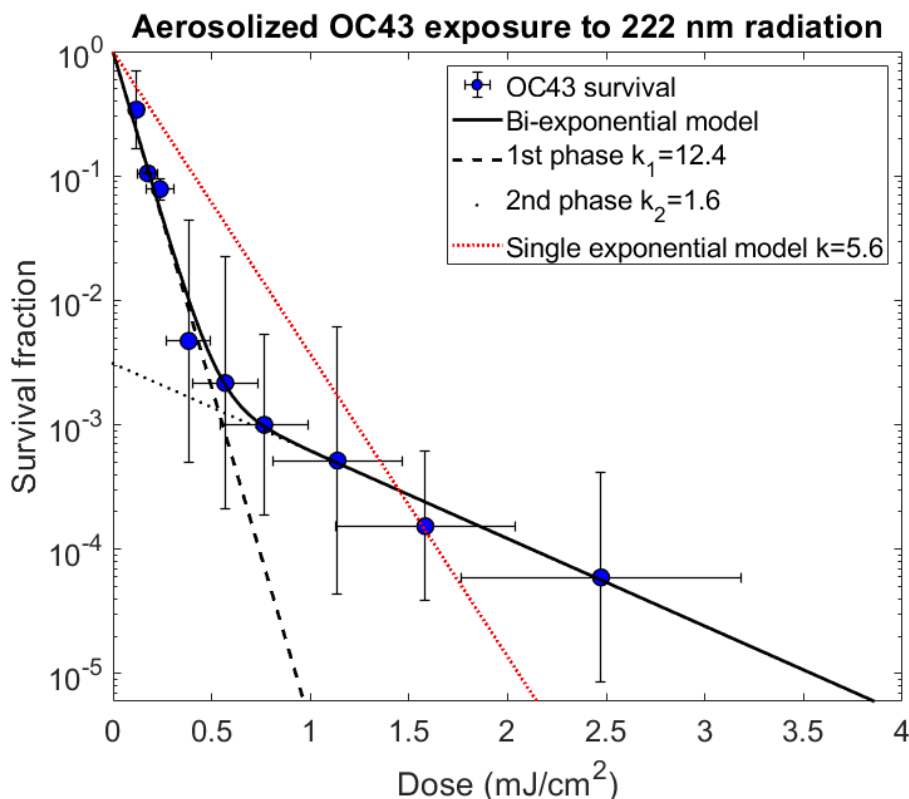
**Table 1.** Summary of exposure conditions and survival results from the exposure of aerosolized HCoV-OC43 to 222 nm radiation. Combinations of mesh screens, their transmission percentage, and the shielding of half of the exposure window permitted the range of exposure doses used for testing. The mean dose with 100% intensity, achieved with full exposure time and no meshes present, was determined using the computational model. The standard deviation is abbreviated as SD.

Mesh on Lamp % Open Area	Mesh on Chamber % Open Area	Exposure time (s)	Percentage of Maximum Radiant Exposure	Mean Dose (mJ/cm <sup>2</sup> )	Survival Fraction	ln(Survival Fraction)	SD ln(Survival Fraction)
None	None	23	100%	2.47	5.94 x10 <sup>-5</sup>	-9.73	1.94
None	64%	23	64%	1.58	1.53 x10 <sup>-4</sup>	-8.78	1.38
None	46%	23	46%	1.14	5.16 x10 <sup>-4</sup>	-7.56	2.46
None	31%	23	31%	0.767	9.99 x10 <sup>-4</sup>	-6.91	1.67
None	46%	11.5	23%	0.569	2.17 x10 <sup>-3</sup>	-6.13	2.34
None	31%	11.5	15.5%	0.383	4.72 x10 <sup>-3</sup>	-5.36	2.24
31%	31%	23	9.61%	0.238	7.82 x10 <sup>-2</sup>	-2.55	0.191
31%	46%	11.5	7.13%	0.176	1.05 x10 <sup>-1</sup>	-2.26	0.0141
31%	31%	11.5	4.80%	0.119	3.40 x10 <sup>-1</sup>	-1.08	0.714

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3.2. Viral Inactivation Results

As described in the Methods section, the susceptibility of aerosolized HCoV-OC43 to inactivation by 222 nm radiation was analyzed using the standard TCID<sub>50</sub> (50% Tissue Culture Infectious Dose) assay [41, 42] to determine the inactivated fraction. Results for the nine exposure doses are shown in Table 1 and Figure 3.



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**Figure 3.** Survival fraction of coronavirus OC43 exposed to 222 nm radiation fitted with the two-phase decay model. The circle markers represent the mean survival values for a given mean exposure dose. The x-error bars show standard deviation of the doses for the 1600 particles in the simulation, and y-error bars show standard deviation of the experimental repeats of survival fraction.



292 The two-phase decay model fit to the data is included on the graph (solid line), as well as lines  
293 representing the decay of the first and second stages separately (dashed and dotted lines, respec-  
294 tively). The single exponential model fit to the same data is included for comparison.

295 The earlier published results [14] on the susceptibility of HCoV-OC43 were fit to a  
296 single-exponential dose-response model (Equation 2). However, the wider range of doses  
297 utilized here allows us to test whether the single-exponential model provided an adequate  
298 fit to the expanded data set, relative to the commonly-used [7] two-phase bi-exponential  
299 model (Equation 1). As described in the Methods, the two models and their fits to the data  
300 were compared using the Akaike information criterion, resulting in an extremely large  
301 difference ( $\Delta\text{AICc} = 47.3$ ); the corresponding very small value of the evidence ratio [ $\exp(-$   
302  $47.3/2) = 5 \times 10^{-11}$ ] indicates that the bi-exponential model provided a significantly better  
303 description of the data than the single-exponential model – in agreement with visual in-  
304 spection of the data in Figure 3.

305 Based on the two-phase bi-exponential model fits, the first phase, representing the  
306 more susceptible fraction of the virus population, had an estimated susceptibility constant  
307 of  $k_1 = 12.4 \pm 0.4 \text{ cm}^2/\text{mJ}$  and described the behavior of approximately 99.7% ( $1-f$ , with  
308  $f = 3.1 \times 10^{-3} \pm 5.4 \times 10^{-4}$ ) of the virus population. The second phase of the bi-exponential model,  
309 representing the less susceptible fraction of the virus population, was found to have an  
310 estimated susceptibility constant of  $k_2 = 1.6 \pm 0.1 \text{ cm}^2/\text{mJ}$  and describes the behavior of  
311  $0.31\% \pm 0.054\%$  of the virus population. By contrast the single exponential fit to the data  
312 yielded a susceptibility constant of  $k = 5.6 \pm 0.9 \text{ cm}^2/\text{mJ}$ . All of the susceptibility constant un-  
313 certainty values reported are standard errors.

#### 314 4. Discussion

315 With far-UVC radiation of increasing interest as a promising technology to limit air-  
316 borne disease transmission in occupied indoor spaces, it is important to be able character-  
317 ize the efficacy of this technology. This study utilized a combination of experimental virus  
318 inactivation data and state-of-the art far-UVC dosimetry to more accurately characterize  
319 the susceptibility of airborne human coronavirus to 222 nm far-UVC radiation.

320 Our earlier study [14] on inactivation of airborne HCoV-OC43 using 222 nm far-  
321 UVC, yielded a single-phase susceptibility constant estimate of  $5.9 \text{ cm}^2/\text{mJ}$ , similar to what  
322 we estimated in the current study ( $5.6 \text{ cm}^2/\text{mJ}$ ) using a single-phase single-exponential  
323 model. However the much narrower spread of doses used in the earlier study [14] pre-  
324 cluded analysis with a two-phase model. In the current study the results, covering a much  
325 wider dose range, clearly showed that a two phase bi-exponential model provided a much  
326 better description of the dose-response data.

327 While observations of a biphasic bi-exponential dose response, in effect the existence  
328 of a small proportion of UV resistant pathogens, are common in the field of ultraviolet  
329 disinfection [7, 48], explanations for this effect are still unclear. In some situations clump-  
330 ing or clustering may provide increased resistance to a subpopulation, since the outer mi-  
331 crobes can act as a photo-protective shield [7, 49]. Recent work by Kowalski *et al.* [48] has  
332 incorporated Mie scattering to model a biphasic dose response related to self-shielding  
333 effects. Alternatively, biphasic dose responses could be caused by a small UV-resistant  
334 subpopulation among the target pathogens. Hiatt [50] commented on deviations from the  
335 single exponential model and grouped the possible explanations as either vitalistic, where  
336 the deviations are due to heterogeneity of the microorganisms, or mechanistic, which at-  
337 tributes deviations to factors during the reactions [50]. However, the overall influence on  
338 the observed bi-exponential response from both vitalistic or mechanistic factors remains  
339 unclear for both experimental setups and real-world implementations.

340 Irrespective, however, of the mechanism(s) underlying the radioresistant fraction,  
341 based on the data analysis here using the two-phase model, we estimate that 99.7% of the  
342 viral population – the more radiosensitive subpopulation – was inactivated with a sus-  
343 ceptibility constant of  $k_1 = 12.4 \text{ cm}^2/\text{mJ}$ , more than twice the susceptibility estimate that was

344 derived using the single-exponential model. This increased susceptibility estimate implies  
345 that a much lower far-UVC dose will be required than previously thought in order to  
346 inactivate the great majority of the airborne aerosolized pathogens in a room environ-  
347 ment. The increased susceptibility also suggests that more virus will be inactivated for a  
348 given dose; therefore, installations of far-UVC, which are dose limited by regulatory  
349 guidelines, will achieve target inactivation doses, *e.g.* a 99.9% inactivation dose, in a  
350 shorter time while operating with the same exposure conditions.

351 Further improvements to estimates of far-UVC efficacy against aerosolized virus  
352 could be beneficial. Tests and simulations which examine effects on virus susceptibility  
353 from variables such as different aerosol sizes or variations in the composition of the sus-  
354 pending media containing the virus would be of interest to real-world disinfection situa-  
355 tions. Additions to the model could also improve the accuracy of the current simulation.  
356 For example, expanding the model to incorporate additional portions of the experimental  
357 chamber prior to the exposure volume could improve the understanding of the expected  
358 particle trajectories through the system, and this could ultimately lead to better dose esti-  
359 mation. Furthermore, additional considerations of effects such as reflection and shadow-  
360 ing by the aerosols on radiation transport would provide information on the possible in-  
361 fluence of these factors on virus susceptibility.

362 In summary, these new results provide added support for the suggestion that far-  
363 UVC could be a highly efficient modality for reducing the level of airborne pathogens in  
364 occupied public spaces. The results suggest that the achievable reduction in airborne path-  
365 ogens - at the low far-UVC exposures which are consistent with current regulatory limits  
366 - will be significantly greater than previously [14, 34] estimated.

367 **Supplementary Materials:** The following supporting information can be downloaded at:  
368 [www.mdpi.com/xxx/s1](http://www.mdpi.com/xxx/s1), Video S1: far\_UVC\_aerosol\_chamber\_simulation.mp4, Figure S1: Normal-  
369 ized spectral irradiance of far-UVC source.

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372 A.G.B, I.S. and D.J.B; investigation, D.W., M.B., A.G.B. and L.Y.; resources, A.G.B, K.D.A. and D.J.B;  
373 data curation, D.W., M.B. and A.G.B.; writing—original draft preparation, D.W. and M.B.; writing—  
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387 **Conflicts of Interest:** D.J.B. has a granted patent entitled – Apparatus, method and system for se-  
388 lectively affecting and/or killing a virus' (US10780189B2), that relates to the use of filtered 222 nm  
389 UV light to inactivate viruses. In addition, D.J.B. has an ongoing non-financial collaboration with  
390 Eden Park Illumination, and the authors' institution, Columbia University, has licensed aspects of  
391 UV light technology to USHIO Inc. The funders had no role in the design of the study; in the collec-  
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